

CUT OF PIEZOELECTRIC OSCILLATOR, PIEZOELECTRIC OSCILLATOR, AND PIEZOELECTRIC DEVICE

RELATED APPLICATIONS

[0001] This application claims priority to Japanese Patent Application No. 2003-076245 filed March 19, 2003 which is hereby expressly incorporated by reference herein in its entirety.

BACKGROUND OF THE INVENTION

[0002] Technical Field

[0003] The present invention relates to a cut of an oscillator making use of a piezoelectric effect and, more particularly, to a cut of a piezoelectric oscillator, piezoelectric oscillator, and piezoelectric device using a so-called new cut quartz plate.

[0004] Related Art

[0005] As various kinds of electronic devices have been advanced and communication systems have evolved in recent years, piezoelectric devices typified by piezoelectric oscillators have been used frequently. Especially, quartz acting as a piezoelectric material has enjoyed wide acceptance in piezoelectric devices, because high frequencies are obtained and stable frequency characteristics are provided. AT-cut quartz plates (hereinafter simply abbreviated AT-cut plates) have been used in piezoelectric devices for a long time because piezoelectric oscillators having stable frequency characteristics in a wide temperature range are obtained. Such an AT-cut plate has one side

parallel to the X axis and has been cut at a cut angle obtained by rotating the XZ-plane with 35.25 degrees in a clockwise direction (as viewed from the -X direction of the X axis to the +X direction) about the X axis.

[0006] In recent years, however, as oscillators and so on have been packed at increasing densities, the operating temperatures have been elevated. Also, it has become necessary to set the operating temperatures of the oscillators higher. Therefore, a double-rotation oscillator whose cut angles are rotated about two axes has been devised instead of the conventional AT-cut oscillator.

[0007] If a quartz plate (double-rotation substrate) cut out with cut angles rotated relative to two axes among the crystallographic axes (electric axis, mechanical axis, and optic axis) of quartz is used, it has been theoretically demonstrated that the central temperature of the frequency-temperature characteristics shifts to the higher temperature side. In a temperature range of from - 25° to + 100°C, cut angles providing stable frequencies exist (for example, see Japanese Patent No. 3,218,537).

[0008] The double-rotation substrate can provide stable frequency-temperature characteristics in this way. At the same time, many spurious oscillations occur compared with the main oscillations. Many frequency jumps or resistance value increases occur due to mechanical oscillation coupling of spurious oscillations with the main oscillations. Many of the spurious oscillations are contour oscillations depending on the longer or shorter sides of blanks or are modes of combinations of them. Accordingly, when a blank is designed, its shape must be determined carefully such that no spurious oscillations exist near the frequency of the main oscillations.

[0009] The temperature characteristics of the double-rotation oscillator are as shown in Fig. 3 when the frequency-temperature characteristics in the temperature range from - 25°C to + 100°C of the oscillator are taken which has rotated with 34.9 degrees about the X axis after rotating 10 degrees about the Z axis, for example. In the figure, the dotted line indicate the frequency-temperature characteristics of the conventional AT-cut oscillator. It can be seen that the double-rotation oscillator shows more stable frequency-temperature characteristics in higher temperature regions as compared to the AT-cut oscillator. In this double-rotation oscillator, the frequency-temperature characteristics have a point at which the gradient of the tangential line is 0 near approximately 25°C in the case of the AT-cut. The temperature at this point is hereinafter referred to as the central temperature. In contrast, the double-rotation oscillator has the phenomenon that the central temperature varies from 25°C to 100°C or higher depending on the rotational angle ϕ .

[0010] The characteristics of the double-rotation oscillator described so far are useful. However, more spurious oscillations (undesired oscillations) having other modes of oscillations are produced than the conventional AT-cut oscillator. For example, contour oscillations depending on the longer and shorter sides of the blank vary in frequency due to deviation in blank contour. Therefore, if the frequency comes too close to that of the main oscillations, both oscillations are mechanically coupled, causing jumps in the frequency of the main oscillations or resistance increases. Similarly, in the temperature range of from -25°C to 100°C taken as operating temperatures, spurious oscillations occur at certain temperatures near the main oscillations. This produces the phenomenon that the frequency of the main oscillations deviates or the

resistance value increases. Similar phenomena are observed with AT-cut oscillators. Especially, in the case of double rotations, these phenomena occur frequently. The present inventors have investigated the cause using an analytical method known as the finite element method.

[0011] As a result, we have found that the cause is the direction of displacement of thickness shear oscillation that is the main oscillation. The conventional AT-cut oscillator produces a thickness shear oscillation whose direction of displacement is only in the X-direction. On the other hand, the direction of displacement of the double-rotation oscillator has all of the components of X, Y, and Z. The phenomenon of a frequency shift or resistance increase caused by spurious oscillations is due to the fact that the main and spurious oscillations have common displacement components and thus cause coupling of oscillations (resonance). That is, the main oscillations of the AT-cut oscillator couple with oscillations having only X-direction displacement components. However, the double-rotation oscillator has displacement components of three directions and so there arises the possibility that coupling with the majority of spurious oscillations occurs.

SUMMARY

[0012] The present inventors have calculated the displacement vector on the surface of a double-rotation cut quartz blank, i.e., within the plane formed by the X' axis and Z' axis and produced a clockwise in-plane rotation about the Y' axis such that the X'' axis extends along the direction of displacement vector. A new rectangular blank has been cut so that both sides are parallel to the resulting new X'' axis and Z'' axis, respectively.

[0013] That is, the present invention provides a cut of a piezoelectric oscillator comprising a quartz plate made of a quartz having an electric axis lying on an X axis, a mechanical axis lying on a Y axis, and an optic axis lying on a Z axis, the plate having a side parallel to an X' axis established by rotating the X axis in a clockwise direction about the Z axis with an angle of from 3 degrees to 30 degrees, the quartz plate further having a side parallel to a Z' axis obtained by rotating the Z axis about the X' axis in the clockwise direction with an angle of from 33 degrees to 36 degrees. This cut of a piezoelectric oscillator is characterized in that the quartz plate has sides parallel to X'' axis and Z'' axis, respectively, which have been rotated with angles of from - 35 degrees to - 2 degrees in the clockwise direction about the Y axis that is the thickness direction of the cut of the piezoelectric oscillator.

[0014] In the cut of a piezoelectric oscillator according to the present invention, the frequency of the main oscillations is stable against various shapes and hardly varies even if spurious oscillations come close to the main oscillations. The possibility that frequency jumps or resistance increases take place is low.

[0015] In the present invention, "clockwise direction about an axis" is a direction taken from the negative side to the positive side of the axis. Accordingly, "clockwise direction about the Z axis" means "clockwise direction as viewed from the - Z direction to the + Z direction".

[0016] A piezoelectric oscillator according to the present invention consists of any one of the above-described cuts of a piezoelectric oscillator and can provide improved stability of frequency against machining errors of the longer and shorter sides of a blank. In addition, a piezoelectric oscillator having

a stable frequency in a wide temperature range of from - 25°C to + 100°C is obtained.

[0017] Also, a piezoelectric device according to the present invention is characterized in that it is fitted with the above-described piezoelectric oscillator. As a result, more machining errors are tolerated in mass production steps, and a stable frequency is obtained. Consequently, where the temperature range used is wide as in automobile parts, the frequency can be stabilized without the need of a temperature compensation circuit. The cost can be decreased by avoiding increases in the number of components and number of manufacturing steps.

BRIEF DESCRIPTION OF THE DRAWINGS

[0018] Fig. 1 is an explanatory view of double-rotation cut angles forming the basis of embodiments of the present invention.

[0019] Fig. 2 is an explanatory view of a cut angle according to an embodiment of the invention.

[0020] Fig. 3 shows the frequency-temperature characteristics of a double-rotation oscillator with $\phi = 10^\circ$ and $\theta = 34.9^\circ$.

[0021] Fig. 4 is a diagram illustrating the direction of displacement of main oscillations on the plane of the double-rotation oscillator.

[0022] Fig. 5 is a graph showing the relation between the rotational angle ϕ about the Z axis and the deviation γ of displacement from the direction of the longer sides.

[0023] Fig. 6 shows the relation between the Z side ratio and frequency in a case where the direction of displacement is parallel to the

direction of the longer sides.

[0024] Fig. 7 shows the relation between the Z side ratio and frequency in a case where the direction of displacement deviates 8 degrees from the direction of the longer sides.

[0025] Fig. 8 shows the relation between the Z side ratio and frequency in a case where the direction of displacement deviates 16 degrees from the direction of the longer sides.

[0026] Fig. 9 is a frequency distribution of variations in main oscillation frequencies of various shapes in a case where the direction of displacement is parallel to the direction of the longer sides.

[0027] Fig. 10 shows the frequency distributions of variations in the main oscillation frequencies of various shapes in the case where the direction of displacement deviates 8 degrees from the direction of the longer sides.

[0028] Fig. 11 shows the frequency distributions of variations in the main oscillation frequencies of various shapes in the case where the direction of displacement deviates 16 degrees from the direction of the longer sides.

[0029] Fig. 12 is a diagram showing the frequency-temperature characteristics of a cut of a quartz oscillator according to the invention under conditions of $\phi = 10^\circ$, $\Omega = -8.0^\circ$, and $\theta = 34.85^\circ$.

[0030] Figs. 13(A) and 13(B) are explanatory views of a piezoelectric oscillator according to an embodiment. Fig. 13(A) is a cross-sectional view taken along line B-B of Fig. 13(B), and Fig. 13(B) is a cross-sectional view taken along line A-A of Fig. 13(A).

DETAILED DESCRIPTION

[0031] The preferred embodiments of cut of a piezoelectric oscillator, piezoelectric oscillator, and piezoelectric device according to the present invention are described in detail with reference to the accompanying drawings.

[0032] Figs. 1 and 2 are views illustrating cut angles of quartz for obtaining a cut quartz oscillator that is a cut of a piezoelectric oscillator according to the present invention. In Fig. 1, three axes of a quartz crystal 10 crossing perpendicularly to each other, i.e., electric axis, mechanical axis crossing perpendicularly to the electric axis, and optic axis crossing perpendicularly to those axes are taken as X axis, Y axis, and Z axis, respectively. With respect to the cut angles of the double-rotation cut-angled quartz plate (quartz substrate) 11 defined in the present invention, an X' axis obtained by rotating the X axis about the Z axis with merely ϕ in a clockwise direction is first established. The plate has sides parallel to the X' axis. Furthermore, the quartz plate 11 has sides parallel to a Z' axis obtained by rotating the Z axis in the clockwise direction with merely θ about the X' axis.

[0033] A cut of quartz 12 according to the invention is a cut of quartz having sides parallel to an X'' axis and a Z'' axis obtained by rotating the quartz plate 11 about the Y' axis with merely angle Ω as shown in Fig. 2. In this figure, + direction of the Y' axis is a direction directed from the rear surface of the paper to the front.

[0034] The present inventors have conducted various discussions on the cut angles of the quartz crystal 10 which have been rotated about the X axis, Z axis, and Y' axis and have found that the present cut-angled oscillator suffers from less frequency jumps and resistance increases due to spurious

oscillations in various forms than the conventional double-rotation oscillator. Furthermore, the temperature characteristics are more stable.

[0035] As shown in Fig. 4, the calculated result of the direction of displacement of the main oscillations on the double-rotation cut quartz 11 reveals that the direction of displacement of the main oscillations is not parallel to the direction of the longer side on the X'' axis but has a deviation angle γ as indicated by the arrow in the figure. Fig. 5 shows the computationally derived results of the direction of displacement of the main oscillations on the double-rotation cut quartz 11 when the rotational angle ϕ about the Z axis is varied. The lateral axis indicates the rotational angle ϕ about the Z axis, while the vertical axis indicates the deviation γ in the direction of displacement. These are represented by defining the clockwise direction relative to the $+Y'$ axis as positive (+). As can be seen from the figure, as the rotational angle ϕ increases, the deviation γ between the X' axis and the direction of displacement increases in one direction.

[0036] Accordingly, the blank is rotated about the Y' axis within the plane formed by the X' axis and Z' axis with merely γ such that the direction of the longer sides of the blank becomes parallel to the direction of displacement of the main oscillations.

[0037] This rotational angle is Ω . For example, the degrees of the deviation of the frequency of the main oscillations due to spurious oscillations were calculated for a case where the direction of displacement is parallel to the direction of the longer sides and for a case where the direction of displacement is not parallel. Also, the degrees of increase in the resistance value were calculated. It is now assumed that the sides parallel to the X'' axis are the

longer sides and that the sides parallel to the Z'' axis are the shorter sides. The results are shown in Figs. 6-8. The lateral axis of each figure is the Z side ratio, i.e., the length of the shorter sides of the blank divided by the thickness of the quartz. The vertical axis indicates the frequency. Here, ϕ is 20 degrees, and the longer sides of the blank has a constant length of 2.0 mm. In the figures, the frequency positions of main oscillations are indicated by the white dots. The frequency positions of spurious oscillations are indicated by the black dot group. The size of each dot corresponds to the intensity of each oscillation. A larger dot indicates a stronger oscillation. For example, the lines in Fig. 6 indicate the motion of a certain spurious oscillation. As the Z side ratio of the blank increases, the spurious position shifts to the lower frequency side. It can be understood, on the other hand, that the main oscillations are almost constant regardless of the Z side ratio and that when the spurious oscillations are approached, the frequency shifts greatly due to oscillation coupling. At the same time, the dots of the spurious oscillations increase in size. Hence, it can be inferred that the oscillation intensities increase compared with the main oscillations. At this time, the main oscillations are deprived of their oscillation energies by spurious oscillations and so the oscillation intensities of the main oscillations decrease. That is, the resistance values of the main oscillations increase.

[0038] The figures are compared. Fig. 6 shows a case where the direction of displacement is made parallel to the direction of the longer sides of the blank. The rotational angle Ω about the Y' axis is - 8 degrees. Fig. 7 shows a case where Ω is 0, i.e., the direction of the longer sides deviates 8 degrees from the direction of displacement at the double-rotation cut angle. Fig. 8

shows a case where Ω is 8 degrees and the direction of the longer sides deviates 16 degrees from the direction of displacement. It can be seen from the comparison of the three figures that the frequency shifts are small and spurious oscillations are not so strong in Fig. 6 where the direction of displacement is parallel to the direction of the longer sides. However, as can be seen from Figs. 7 and 8, as the deviation from the parallel relation between the direction of displacement and the direction of the longer sides increases, variation width of frequency increases, and the oscillation intensity of the whole spurious oscillation increases.

[0039] After checking these facts computationally, oscillators using cuts of quartz according to the present invention were prototyped under conditions of ϕ of 20 degrees and θ of 34.0 degrees. Double-rotation cut-angled quartz oscillators of this construction were rotated about the Y' axis with angles Ω of - 8 degrees, 0 degrees, and 8 degrees, respectively. The longer and shorter sides of each blank were made parallel to the X'' axis and Z'' axis after rotation within the plane. In the present prototypes, the longer sides were kept constant. Each shorter side was varied by varying the Z side ratio from 15.0 to 17.0, and the frequency of the main oscillations of each cut oscillator was measured.

[0040] Figs. 9, 10, and 11 represent the frequency distributions of the results of the measurements described above. In Fig. 9, the direction of displacement of the main oscillations is parallel to the direction of the longer sides. In Fig. 10, the direction of the longer sides deviates 8 degrees from the direction of displacement. In Fig. 11, the deviation is 16 degrees. In Fig. 9, frequency variations are smaller than in Figs. 10 and 11. Also, the variation

width increases with increasing deviation, for the causes considered below. As the deviation from the parallel relation increases, many oscillational couplings with spurious oscillations occur in various shapes, causing jumps of the frequency of main oscillations. Because of these results, it can be seen that a stable frequency is obtained irrespective of the shape of the cut oscillator by making the direction of the longer sides parallel to the direction of displacement.

[0041] The frequency-temperature characteristics of the cut oscillators according to the invention were measured. The results are shown in Fig. 12. A stable frequency of main oscillations can be obtained over a wide temperature range comparable to the frequency-temperature characteristics of the double-rotation oscillator shown in Fig. 3. It has been confirmed that rotation about the Y' axis hardly affects the temperature characteristics.

[0042] The results above show that in the double-rotation cut-angled oscillator, displacement of the main oscillations is not parallel to the direction of the longer sides and so coupling with spurious oscillations existing thereabout easily occurs. As a result, frequency jumps and resistance value increases occur easily. To avoid them, it is desirable to rotate Ω within the range from -35 degrees to -2 degrees within the plane at the cut angle of double rotation. However, where ϕ is less than 3 degrees, the direction of displacement is almost parallel to the direction of the longer sides and so in-plane rotation about the Y' axis is not necessary. Where ϕ is greater than 30 degrees, the central temperature of the temperature characteristic curve becomes too high with impractical results. Therefore, the range of ϕ from 3 degrees to 30 degrees is desirable. In this range of ϕ , the range of θ in which the gradient of the tangential line to the temperature characteristic curve is 0 near the central

temperature is greater than 33 degrees and less than 36 degrees as given by

[0043] Equation 2

$$-35 \leq \Omega \leq -2$$

wherein, $3.0 \leq \phi \leq 30$

$$33.0 \leq \theta \leq 36.0$$

[0044] Especially,

[0045] the relation between ϕ and Ω that satisfies the function of Eq. (3) shown in Fig. 5 is considered to be the optimum condition. However, the region in which the frequency-temperature characteristics of the double-rotation cut oscillator are good differs slightly depending on the side ratio and on the amount of plateback using the electrodes. This causes a deviation of the optimum region of Ω . Therefore, the width of ± 3 degrees of the value of the Ω derived from Eq. (3) is the optimum region in practice. This is given by Eq. (4).

[0046] Equation 3

$$\Omega^\circ = (-0.0037 \times \phi^3 + 0.1106 \times \phi^2 - 1.161 \times \phi + 0.239)^\circ$$

[0047] Equation 4

$$\Omega^\circ = (-0.0037 \times \phi^3 + 0.1106 \times \phi^2 - 1.161 \times \phi + 0.239 \pm 3)^\circ$$

(wherein, $3.0 \leq \phi \leq 30$)

[0048] The cut of a piezoelectric oscillator (cut of a quartz oscillator) consisting of the quartz plate 12 cut out with the cut angle obtained under the above conditions can be used as a piezoelectric oscillator by hermetically sealing the cut of the oscillator into a package. Fig. 13 gives explanatory views of the piezoelectric oscillator. Fig. 13(A) is a plan view in cross section taken on

line B-B of Fig. 13(B). Fig. 13(B) is a side elevation in cross section taken on line A-A of Fig. 13(A).

[0049] In Figs. 13(A) and (B), a piezoelectric oscillator 20 has a package 22 made of an insulating material such as a ceramic material. The package 22 is provided with a cavity 26 accommodating a cut of a piezoelectric oscillator 24. Electrodes 30 and a wiring pattern (not shown) are formed on the bottom surface of the cavity 26 in the package 22 to permit electrical connection with external terminals (not shown) formed on the rear surface of the package 22. The cut of the piezoelectric oscillator 24 is cantilevered and mounted in the cavity 26. Specifically, conductive adhesive 32 is applied onto the electrodes 30. Connector electrodes 34 of the cut of the piezoelectric oscillator 24 are disposed on the adhesive and made stationary. This makes it possible to electrically energize exciting electrodes 36 of the cut of the piezoelectric oscillator 24 from the external terminals on the bottom surface of the package 22. A cover member 38 is mounted on top of the package 22, and the inside of the package 22 is maintained as a nitrogen ambient or the like.

[0050] The cut of a piezoelectric oscillator according to the present embodiment can be used as a piezoelectric oscillator by combining the cut of the piezoelectric oscillator with integrated circuit elements and forming an oscillator circuit. For example, a piezoelectric oscillator module can be formed by mounting the piezoelectric oscillator 20 shown in Figs. 13(A) and (C) and integrated circuit elements (not shown) on a module substrate on which a wiring pattern has been formed. Furthermore, a piezoelectric oscillator package can be fabricated by hermetically sealing integrated circuit elements into the package 22 shown in Figs. 13(A) and (C) together with the cut of the

piezoelectric oscillator 24.

[0051] The cut of a piezoelectric oscillator according to the invention can be, for example, planar, convex, or inverted mesa form in which the central portion of the cut of the piezoelectric oscillator is recessed.

[0052] Advantages of the Invention

[0053] As described so far, by adopting the cut angle according to the present invention, the frequency of the main oscillations can be stabilized irrespective of various shapes of the cuts of quartz.